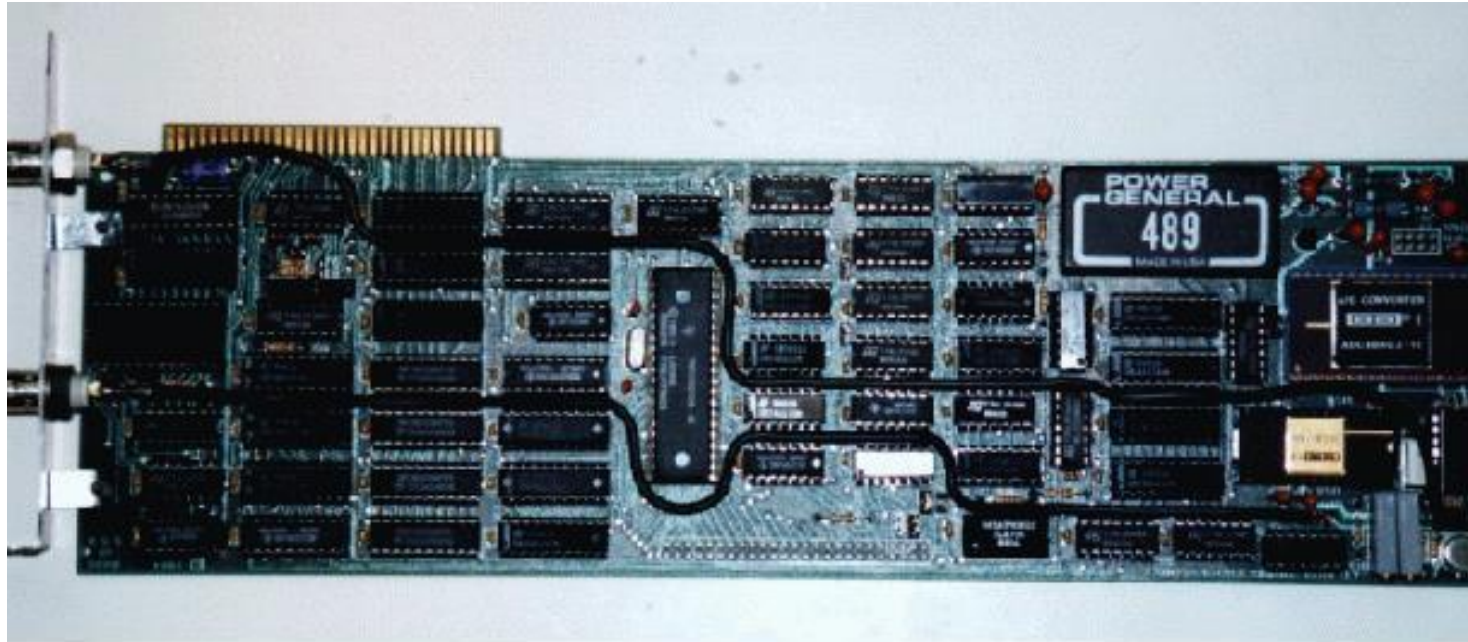


FIR FILTERS IN FREQUENCY

C H A P T E R

6

The TMS32010, 1983



First PC plug-in board from Atlanta Signal Processors Inc.

Rockland Digital Filter, 1971



**Model 4136
PROGRAMMABLE
DIGITAL
FILTER**

Variable-Order Digital Filter for Realizing All Classical Designs

The Rockland Model 4136 Programmable Digital Filter consists of a second-order digital filter section which is multiplexed four ways to achieve eighth-order filtering. Each of the four sections has fully-programmable coefficients which are stored internally in a read-write memory.

Filter input and output words are in 16-bit parallel form at a maximum sampling rate of 80 KHz while internal computations are made with 24-bit ac-

TRANSFER FUNCTION

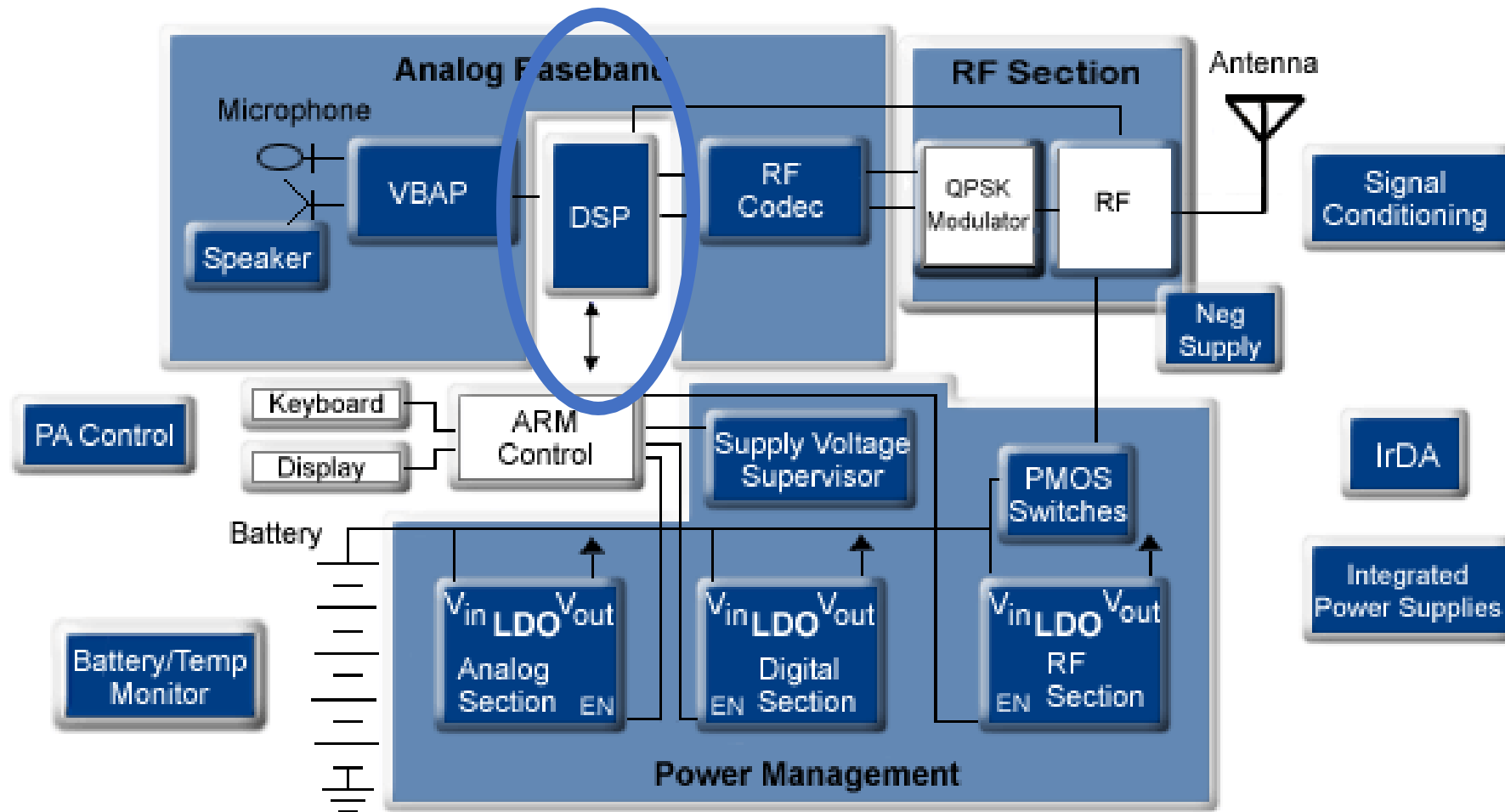
The transfer function from filter input to filter output in z-transform notation is given by

$$H_N(z) = \prod_{n=1}^N \frac{K_n(1+z^{-1}A1,+z^{-2}A2)}{1-z^{-1}B1,-z^{-2}B2} \quad (1)$$

where $N=0,1,2,3,4$ is one-half the filter order se-

Cost was about the same as the price of a small house.

Digital Cell Phone (ca. 2000)



Now, digital cameras and video streaming rely on DSP algorithms

Frequency Response of an FIR System

$$H(e^{j\hat{\omega}}) = \sum_{k=0}^M b_k e^{-j\hat{\omega}k} = \sum_{k=0}^M h[k] e^{-j\hat{\omega}k}$$

(6.4)

Relationship of digital frequency to analog ω /(Sampling Frequency) Page 105

$$\hat{\omega} = \omega T_s = \omega / f_s \quad (\text{Radians} = \text{radians/sec} * \text{Seconds})$$

$$y[n] = \sum_{k=0}^M b_k x[n - k]$$

FILTER OUTPUT

INPUT A SINUSOID (EXPONENTIAL DIGITAL FORM)

$$x[n] = A e^{j\varphi} e^{j\hat{\omega}n} \quad -\infty < n < \infty$$

$$\mathcal{H}(\hat{\omega}) = \sum_{k=0}^M b_k e^{-j\hat{\omega}k} \quad (6.3)$$

TRANSFER FUNCTION

TRANSFER FUNCTION

$$\begin{aligned} y[n] &= \left(|H(e^{j\hat{\omega}})| e^{j\angle H(e^{j\hat{\omega}})} \right) A e^{j\varphi} e^{j\hat{\omega}n} \\ &= (|H(e^{j\hat{\omega}})| \cdot A) e^{j(\angle H(e^{j\hat{\omega}}) + \varphi)} e^{j\hat{\omega}n} \end{aligned} \quad (6.5)$$



AMPLITUDE CHANGE



PHASE CHANGE

The term "**transfer function**" is also used in the frequency domain analysis of systems using transform methods such as the Laplace transform; here it means the amplitude of the output as a function of the frequency of the input signal. **For example, the transfer function of an electronic filter is the voltage amplitude at the output as a function of the frequency of a constant amplitude sine wave applied to the input.**

Measuring frequency response

for $\omega = \omega_1, \dots, \omega_N$,

- apply sinusoid at frequency ω , with phasor \mathbf{U}
- wait for output to converge to SSS
- measure \mathbf{Y}_{ss}
(*i.e.*, magnitude and phase shift of y_{ss})

N can be a few tens (for hand measurements) to several thousand

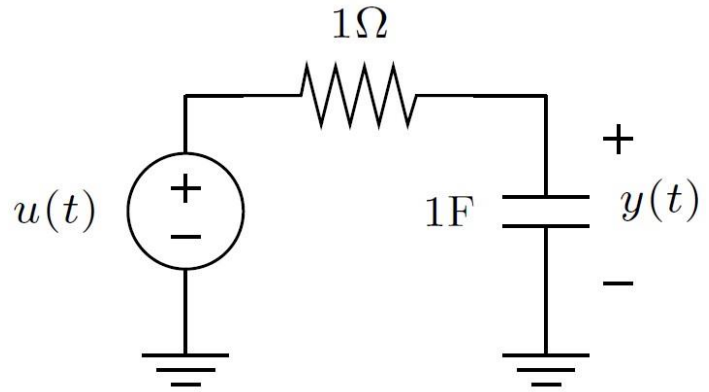
Frequency response plots

- $|H(j\omega)|$ & $\angle H(j\omega)$ versus ω (called *Bode plot*)

the most common format is a Bode plot

<https://www.tutorialspoint.com/low-pass-and-high-pass-filter-bode-plot>

example: RC circuit

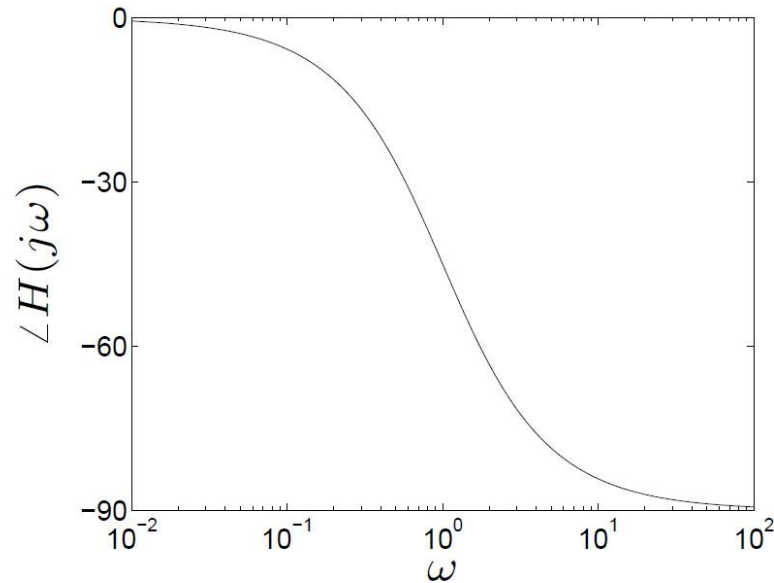
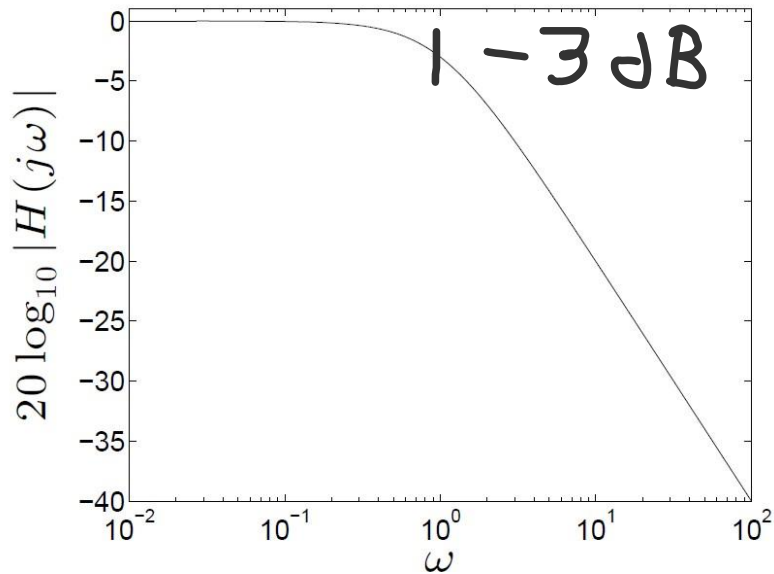


$$Y(s) = \frac{1}{1+s}U(s)$$

R ohm =
C farad =1

$$H(j\omega) = \frac{1}{1+j\omega}$$

A really **BIG** capacitor



WHY -90°

Log scale in radian
frequency

Low Pass Filter Bode Plot

The frequency response function or transfer function of the RC low pass filter is given by,

$$\frac{V_{out}}{V_{in}} = \frac{A}{1 + (j\omega T)} = \frac{A}{1 + (j\omega / \omega_0)} = \frac{A}{\sqrt{1 + (\omega / \omega_0)^2}} \angle -\tan^{-1}\left(\frac{\omega}{\omega_0}\right)$$

Where,

- T = Time constant of the circuit = $1/\omega_0 = RC$
- A = Constant and
- ω_0 = Cut off frequency

Bode Magnitude Plot of LPF

The magnitude plot can be obtained from the absolute value of transfer function i.e.

$$\left| \frac{V_{out}}{V_{in}} \right| = 20 \log_{10} \frac{|A|}{|1 + j\omega / \omega_0|}$$

When $\omega < \omega_0$, then the imaginary part is much smaller than its real part, so $|1 + j\omega / \omega_0| = 1$, thus,

$$\left| \frac{V_{out}}{V_{in}} \right|_{dB} = 20 \log_{10} A - 20 \log_{10} 1 = 20 \log_{10} A$$

Hence, at very low frequencies the frequency response function is approximated by a straight line of zero slope, which is the low frequency asymptote of the Bode plot.

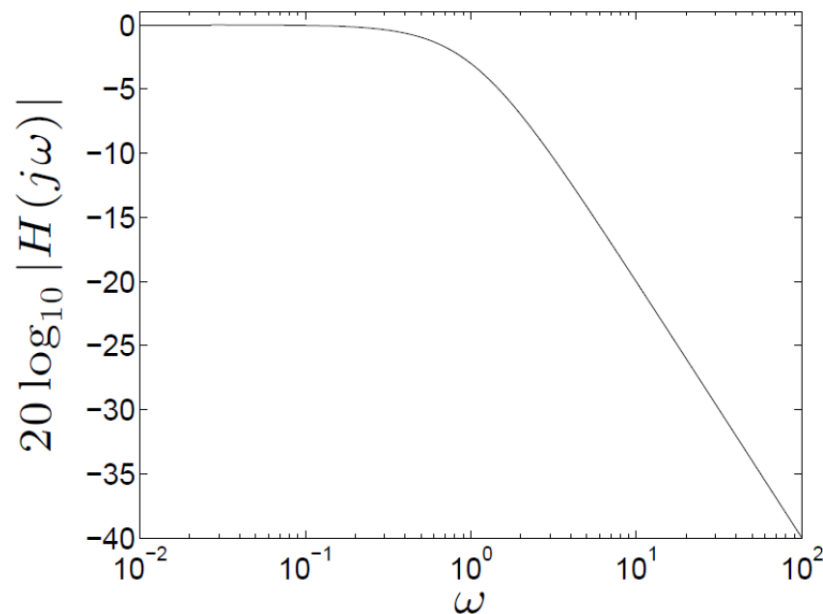
When $\omega > \omega_0$ then the imaginary part is much larger than its real part, so $|1 + j\omega / \omega_0| = |j\omega / \omega_0|$, thus,

$$\left| \frac{V_{out}}{V_{in}} \right|_{dB} = 20 \log_{10} A - 20 \log_{10} (\omega / \omega_0) = 20 \log_{10} A - 20 \log_{10} \omega - 20 \log_{10} \omega_0$$

Hence, at very high frequencies the frequency response function is approximated by a straight line of (- 20 dB / Decade) slope that intercepts the $\log \omega$ at $\log \omega_0$. This line is the high frequency asymptote of the bode plot.

When $\omega = \omega_0$, the real and imaginary part of the simple pole are equal, so $|1 + j\omega / \omega_0| = |1 + j| = \sqrt{2}$, thus,

$$\left| \frac{V_{out}}{V_{in}} \right|_{dB} = 20 \log_{10} A - 20 \log_{10} \sqrt{2} = 20 \log_{10} A - 3dB$$



$$\omega_0 = 1/RC = 1 \text{ rad/sec}$$

Bode Phase Plot of LPF

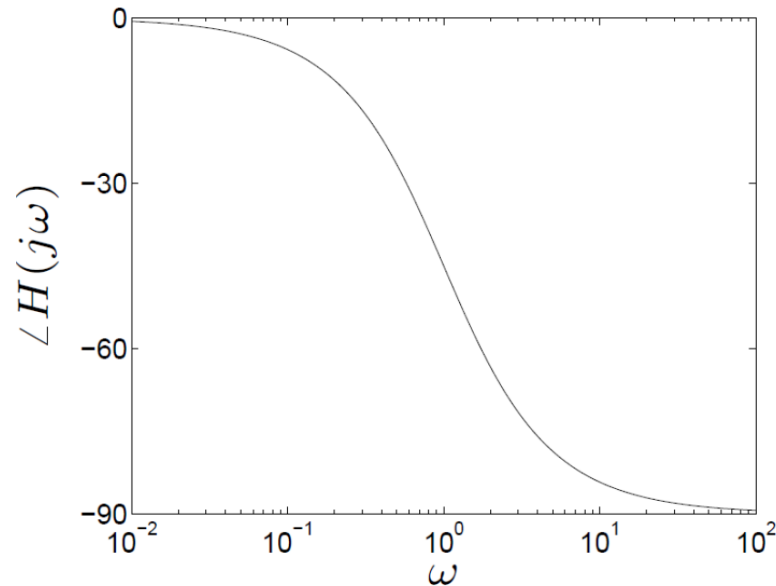
$$\angle\left(\frac{V_{out}}{V_{in}}\right) = -\tan^{-1}\left(\frac{\omega}{\omega_0}\right)$$

When $\omega = 0$, Then

$$\angle\left(\frac{V_{out}}{V_{in}}\right) = -\tan^{-1}\left(\frac{\omega}{\omega_0}\right) = -\frac{\pi}{4}$$

When $\omega \rightarrow \infty$, Then

$$\angle\left(\frac{V_{out}}{V_{in}}\right) = -\tan^{-1}\left(\frac{\omega}{\omega_0}\right) = -\frac{\pi}{2}$$



FIRST ORDER LOW-PASS
FILTER!

WHY -90°

Consider an LTI system for which the difference equation coefficients are $\{b_k\} = \{1, 2, 1\}$. Substituting into (6.3) gives

$$H(e^{j\hat{\omega}}) = 1 + 2e^{-j\hat{\omega}} + e^{-j\hat{\omega}2}$$

To obtain formulas for the magnitude and phase of the frequency response of this FIR filter, we can manipulate the equation as follows:

$$\begin{aligned} H(e^{j\hat{\omega}}) &= 1 + 2e^{-j\hat{\omega}} + e^{-j\hat{\omega}2} \\ &= e^{-j\hat{\omega}} \left(e^{j\hat{\omega}} + 2 + e^{-j\hat{\omega}} \right) \\ &= e^{-j\hat{\omega}} (2 + 2 \cos \hat{\omega}) \end{aligned}$$

Relationship of digital frequency to analog ω /(Sampling Frequency) Page 105

$$\hat{\omega} = \omega T_s = \omega / f_s$$

Suppose there is a dc component of 5 volts = A_0 :

$$H(e^{i\hat{\omega}}) = e^{-i\hat{\omega}} [2 + 2\cos(\hat{\omega})] = e^0 (2 + 2) = 4 \angle 0 \text{ Degrees ;}$$

$$Y[n] = H * 5 \text{ Volts} = 4 * 5 = 20 \text{ volts } \angle 0 \text{ Degrees}$$

$$1. H(e^{j\hat{\omega}}) = e^{-j\hat{\omega}} (2 + 2 \cos \hat{\omega})$$

DSP/F
EXAMPLE 6.4
Pg 200

$$2. x[n] = 4 + A \cos\left(\frac{7\pi}{8}n\right)$$

$$3. H(e^{j0}) = 1 \cdot (2 + 2) = 4$$

$$4. H(e^{j\frac{7\pi}{8}}) = e^{-j\frac{7\pi}{8}} \left[2 + 2 \cos\left(\frac{7\pi}{8}\right) \right]$$

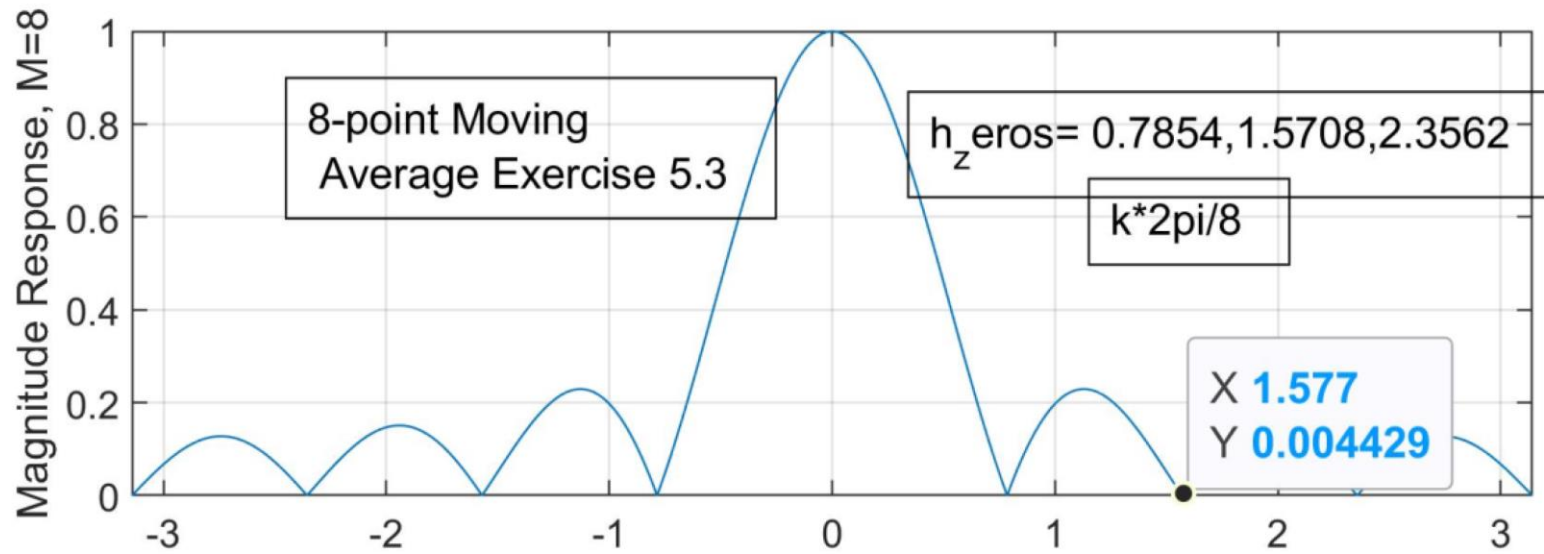
↗ 157.5°

↖ 157.3°

(-.9239)

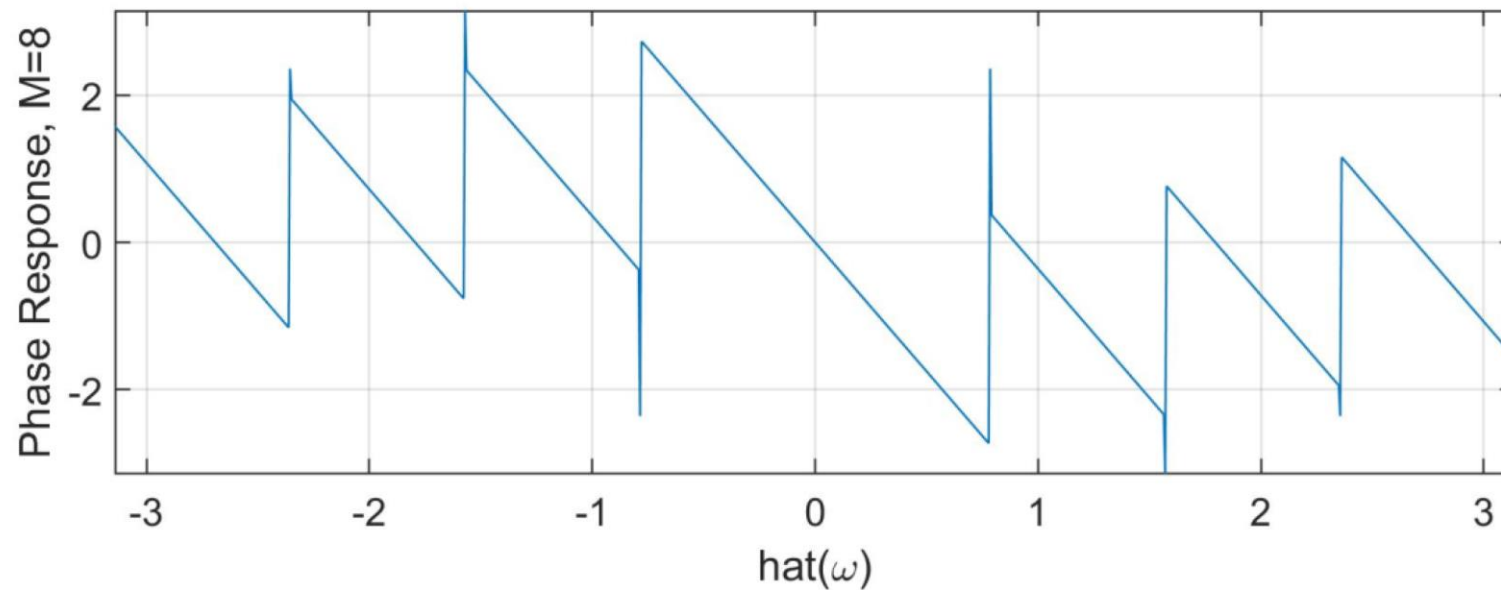
0.1522

So y[n] = 4.4 + A(0.1522) cos $\left[\frac{7\pi}{8}n - \frac{7\pi}{8} \right]$



DSPF Pg 214 & 220

Zeros: $k (2 \pi/8)$
 $\pi/4, \pi/2, 3 \pi/4$



```
% 8-point Moving Average Frequency Response
% Exercise 5.3
clc, clear all, clf
w_hat=-pi:pi/500:pi;
H_8=freqz(ones(1,8)/8,1,w_hat);
h_8zeros= (1/8)*[2*pi,4*pi,6*pi]
% h_8zeros = 0.7854      1.5708      2.3562
figure(1)
subplot(211)
plot(w_hat,abs(H_8))
grid;axis([-pi pi 0 1])
ylabel('Magnitude Response, M=8')
subplot(212)
plot(w_hat,angle(H_8))
grid;axis([-pi pi -pi pi]);
ylabel('Phase Response, M=8')
xlabel('hat(\omega)')
```