

## Z plane & S to Z and H(z) 4/15

**Introduction to Z-Transforms** We now turn to a transform that is called the *Z-transform* due to the use of the complex variable  $z = x + iy$  in the transform. The *Z-transform* plays the same role for discrete systems as the Laplace transform does for continuous systems. The table summarizes some of the applications of the *Z-transform*.

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Definition	The <i>Z-transform</i> is defined as a sum that transforms discrete signals to the complex frequency ( <i>Z</i> ) domain.
System analysis	The <i>Z-transform</i> converts convolutions to a product and difference equations to algebraic equations.
Stability	Stability of a discrete linear system can be determined by analyzing the transfer function $H(z)$ given by the <i>Z-transform</i> .
Frequency response	The transfer function $H(z)$ can be evaluated to determine the frequency response of a discrete system.
Digital filters	Digital filters can be analyzed and designed using the <i>Z-transform</i> .
Control	Digital control systems can be analyzed and designed using <i>Z-transforms</i> .

We shall see that there is a close connection between the *Z* and Laplace transforms.

**The Z-plane and the s-plane Laplace and Z-Transforms** In this section, the term *sampling* refers to replacement of a function  $f(t)$  by the function  $f(nT)$ . Here we consider *sampled-data* systems in which input and output functions are considered at only discrete values of  $t$ , usually at values  $nT, n = 0, 1, 2, \dots$ , where  $T$  is a positive constant.

By sampling the continuous function  $f(t)$  at every  $T_s$  seconds, we obtain the discrete function  $f_d(t)$  with values defined at  $t = 0, T_s, 2T_s, \dots$ . This discrete function can be written in terms of the unit impulse function

$$\delta(t - nT_s) = \begin{cases} 1, & t = nT_s \\ 0, & t \neq nT_s \end{cases} \quad (1)$$

where  $n = 0, 1, \dots$  in the following manner:

$$f_d(t) = \sum_{n=0}^{\infty} f(nT_s) \delta(t - nT_s). \quad (2)$$

The discrete time function  $f_d(t)$  has as its Laplace transform

$$\begin{aligned} \mathcal{L}[f_d(t)] &= \int_0^{\infty} \sum_{n=0}^{\infty} f(nT_s) \delta(t - nT_s) e^{-st} dt \\ &= \sum_{n=0}^{\infty} f(nT_s) e^{-nT_s s} \end{aligned} \quad (3)$$

using the definition of the one-sided Laplace transform and the properties of the impulse function.

Defining a new complex variable

$$z = e^{T_s s}$$

leads to the definition of the  $Z$ -transform as the Laplace transform of the discrete function  $f(nT_s)$

$$\mathcal{L}[f(nT_s)] = \sum_{n=0}^{\infty} f(nT_s) z^{-n} = F(z). \quad (4)$$

**ZtoS** From the relationship

$$z = e^{sT_s} = e^{(\sigma+i\omega)T_s} = e^{\sigma T_s} e^{i\omega T_s} \quad (5)$$

we map the  $s$ -plane into the  $z$ -plane. The  $i\omega$  axis maps into the unit circle

$$z = e^{i\omega T_s}$$

which has magnitude  $|z| = 1$ . The values of  $i\omega T_s$  determine the position on the circle. As the argument increases in the positive direction, points on the circle wrap around starting at  $z = 1$  when  $\omega T_s = 0$  corresponding to  $\omega = 0$  in the  $s$ -plane. At the angle  $\omega T_s = \pi$ ,  $z = -1$ . The region of the  $j\omega$  in the  $s$ -plane axis from  $\omega = 0$  to  $-\omega T_s = -\pi$  map to the lower half of the unit circle and again  $z = -1$  when  $-\omega T_s = -\pi$ .

In terms of sampling theory, the limits used to preserve the uniqueness of the mapping correspond to the Nyquist frequencies  $\omega_s = \pm\pi/T_s$ .

**Damping and the  $z$ -plane** The left-hand side of the  $s$ -plane, for values  $s = \sigma + i\omega$  with  $\sigma < 0$  and  $|\omega| < \pi/T_s$  maps into the interior of the unit circle in the  $z$ -plane. Since poles in the left-hand  $s$ -plane correspond to a BIBO stable continuous system, the corresponding poles for stable discrete systems must lie within the unit circle in the  $z$ -plane. Note that the negative real axis in the  $s$ -plane maps into the real axis from 0 to 1 in the  $z$ -plane. Thus, a digital system with a pole at  $-0.5$ , for example, has no corresponding continuous system. (Shahian p 263).

If  $\sigma > 0$ , the points in the right-hand  $s$ -plane map to the exterior of the unit circle in the  $z$ -plane.

Vertical lines in the  $s$ -plane such that  $\pi/T_s \leq \omega \leq \pi/T_s$  and  $\sigma < 0$ , map into a circle in the  $z$ -plane centered at  $z = 0$  with radius  $r = \exp(\sigma T_s)$ .

**Mapping the  $s$ -plane to the  $z$ -plane** Consider the  $s$ -domain function

$$G(s) = \frac{1}{(s+1)(s+2)(s^2+1)}$$

with poles at  $s = -1, -2, \pm i$ . For  $T_s = 1$ , the poles in the  $z$ -plane given by  $\exp(sT_s)$  appear at

$$z = 0.3679, 0.1353, 0.5403 + 0.8415i, 0.5403 - 0.8415i$$

as computed by the MATLAB script below and shown in Figure ??.

The inverse Laplace transform of  $G(s)$  leads to time functions such as  $e^{-t}, e^{-2t}$  and  $e^{\pm it}$  or  $\cos t$  and  $\sin t$ . Thus, the oscillations have frequency  $f = 1/2\pi$  Hertz or 1 rad/sec. With  $T_s = 1$ ,  $\omega_s = 2\pi$  and the maximum digital frequencies are  $F = .5$  or  $\Omega = \pi$  radians.

In the  $z$ -plane, the pole at  $0.5403 + 0.8415i$  has magnitude 1 since it lies on the unit circle and angle

$$\theta_z = \tan^{-1} \frac{0.8415}{0.5403} = 1 \text{ radian.}$$

With  $T_s = 1$ , the maximum digital frequency  $\Omega = \pi$  rad occurs at the point  $z = -1$ .

If  $T_s = 0.1$ , the poles in the  $z$  plane are changed as indicated in the results of the MATLAB calculation. The maximum digital frequency is  $F = 5$  or  $\Omega = 10\pi$  radians. The angle of the pole  $z = 0.9950 + 0.0998i$  is  $\theta_z = 0.1000$  radians as expected.

```
%s2zplane.m
% Plot z-plane poles for G(s)=1/[(s+1)(s+2)(s^2+1)
% See Taylor p252
%
% Let Ts=1.0
Ts=1.0
poless=[-1 -2 +i -i]
polesz=exp(poless*Ts)
%
% Define zeros and poles as column vectors
zplane(polesz') % There are no zeros
title('Z-plane for s-plane poles -1,-2,+1=-i')
grid
%
% Results
%
%Ts = 1
%poless =-1.0000 -2.0000 0 + 1.0000i 0 - 1.0000i
%polesz =0.3679 0.1353 0.5403 + 0.8415i 0.5403 - 0.8415i
%
```

```

% Change sampling time
%
%Ts1 = 0.1000
Ts1=0.1
poless1=[-1 -2 +i -i]
polesz1=exp(poless1*Ts1)
% polesz1 =-1.0000  -2.0000      0 + 1.0000i      0 - 1.0000i
% polesz1 = 0.9048  0.8187  0.9950 + 0.0998i  0.9950 - 0.0998i

```

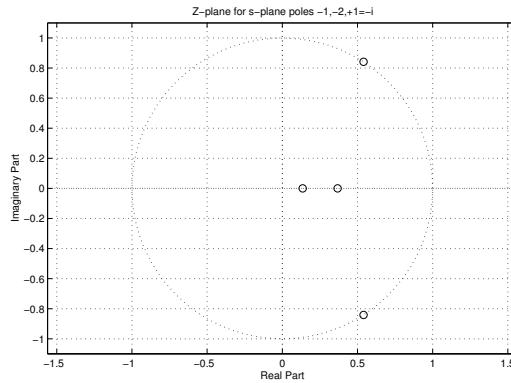


Figure 1:  $z$ -plane poles from  $s$ -plane

**Second-order systems** Consider the second-order system

$$G(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

with poles at

$$s_1 = -\zeta\omega_n + i\omega_n\sqrt{1 - \zeta^2} \quad s_2 = -\zeta\omega_n - i\omega_n\sqrt{1 - \zeta^2}.$$

The term  $\sigma = -\zeta\omega_n$  is the real part of a pole in the  $s$ -domain that corresponds to damping of the time response of the system  $G(s)$ . The pole in the  $z$ -plane lies on a circle centered at  $z = 0$  with radius

$$|z| = \exp(-\zeta\omega_n T_s).$$

**Z-transforms and Frequency Response** We wish to determine the frequency response from the transfer function given by the  $Z$ -transform of  $y(n)$ .

If the transfer function  $H(z)$  is evaluated for values of

$$z = \exp(i2\pi F) = \exp(i\Omega) \tag{6}$$

we obtain the *frequency response*,  $H(i2\pi F)$ , of the system. This is equivalent to evaluating  $H(z)$  on the unit circle in the  $z$ -plane. Note that the function

$H(i2\pi F)$  is periodic with period 1 since  $\exp(i2\pi F)$  is periodic with period 1. The *digital frequency* is defined as

$$F = \frac{f}{f_s} = fT_s,$$

where  $T_s$  is the sampling time or time between samples. The sampling rate  $S = f_s = 1/T_s$  samples per second is often quoted in Hz since then it is easier to compare to the analog frequency given in Hertz.

The analog frequency  $f = 1/T_s$  corresponds to the digital frequency  $F = 1$  or  $\Omega = 2\pi$ . However considering sampling theory, the range of  $F$  is limited as

$$-0.5 \leq F \leq 0.5 \text{ and } -\pi \leq \Omega \leq \pi$$

since  $F = 0.5$  indicates that the sampling rate is twice the analog frequency being sampled. From Equation 6, we have the following correspondences

$$\begin{array}{lll} f=\text{dc} & F = 0 & z = 1 \\ f = S/4 & F = 1/4 & z = i \\ f = S/2 & F = 1/2 & z = -1 \end{array}$$

Note for the equation

$$H(z) = \frac{0.1z}{z - 0.9} \quad (7)$$

for example,

$$H(z = 1) = 0.1(1)/0.1 = 1$$

is the attenuation at the dc value of  $f = 0$ . Notice that  $S$  is not relevant here. However, if  $f = S/2$ , the result becomes

$$H(z = -1) = \frac{0.1(-1)}{-1 - 0.9} = 0.0526$$

which indicates a low-pass filter characteristic. Writing Equation 7 as

$$H(z) = \frac{Y(z)}{X(z)} = \frac{0.1}{1 - 0.9z^{-1}},$$

the difference equation becomes

$$y[n] = 0.9 y[n - 1] + 0.1x[n].$$

Check this with  $x[n] = 1$  for  $n \geq 0$  comparing the step response of  $H(z)$  as

$$y[n] = 1 - (0.9)^{n+1} \quad (8)$$

with the difference equation solution Equation 8 for various values of  $n$  as for example

$$y[0] = 0.9y[-1] + 0.1x[0] = 0.1 \quad (9)$$

$$y[1] = 0.9[0.1] + 0.1 = 0.19 \quad (10)$$